

* Design of Simply Supported Beam:

* Step by step procedure:

Step: ① Determination of required depth:

Step: ② Check for required depth.

Step: ③ Design for flexure

Step: ④ - Curtailment of steel.

Step: ⑤ Check for development length.

Step: ⑥ Check for shear

Step: ⑦ Detailing of reinforcement.

Problem:

A RC rectangular beam of clear span 6m is supported on 300mm wide masonry walls and carries UDL of intensity 30 kN/m. Design the beam and provide all necessary checks and also sketch the reinforcement details? Use M20 mix & HYSD steel.

Solⁿ Given data * Clear span = 6m

* Support width = 300mm

* Working UDL intensity = 30 kN/m

* $f_{ck} = 20 \text{ mpa}$ & $f_y = 415 \text{ mpa}$.

Assume width of the beam 'b' = 300mm.

Self weight of beam per meter = 5 kN/m.

→ Step: ① Determination of Required Depth:

$$= [d_{req}]$$

* Effective span: [Cl: 22.2]

$$\text{Effective span (Left)} = \text{Clear span} + \text{Wall width}$$

$$= 6000 + 300 = 6300 \text{ mm.}$$

$$\begin{aligned} \text{Total UDL intensity} &= W_D + W_L \\ &= 5 + 30 = 35 \text{ kN/m} \end{aligned}$$

$$\text{Factored UDL intensity } (W_U) = 1.5 \times W$$

$$\begin{aligned} \text{Ultimate Bending moment } (M_U) &= 1.5 \times 35 = 52.5 \text{ kN/m} \\ &= \frac{W_U \times l_{\text{eff}}^2}{8} \end{aligned}$$

$$\text{We have, } M_U = 0.138 f_{ck} b d^2 \Rightarrow \frac{52.5 \times 6.3^2}{8} = 260.46 \text{ kN}$$

$$d_{\text{req}} = \sqrt{\frac{M_U}{0.138 f_{ck} b}}$$

$$\Rightarrow d_{\text{req}} = \sqrt{\frac{260.46 \times 10^6}{0.138 \times 20 \times 300}}$$

$$\Rightarrow d_{\text{req}} = 560.86 \text{ mm}$$

$$\therefore \text{Adopt } d = 600 \text{ mm}; D = d + d'$$

$$\Rightarrow D = 600 + 50 = 650 \text{ mm}$$

$$\begin{aligned} \text{Self weight of beam} &= 0.3 \times 0.65 \times 25 \\ &= 4.875 \text{ kN/m} < 5 \text{ kN} \end{aligned}$$

Hence OK

Step: ② Check for required Depth: [Cl: 23.2]

$$L/d \leq k_1 \times k_2 \times k_3 \times k_4 \times k_5$$

$$\text{Where } L = 6000 \text{ mm}$$

$$d = 600 \text{ mm}$$

$$k_1 = 20 \text{ [for simply supported beam]}$$

$$k_2 = 1 \text{ [for span } < 10 \text{ m]}$$

$$k_3 = k_4 = 1 \text{ [Assume]}$$

$$k_5 = 1 \text{ [for rectangular section]}$$

$$\Rightarrow \frac{10}{6000} \leq 20 \times 1 \times 1 \times 1 \times 1$$

$$\Rightarrow 10 \leq 20 \text{ Hence ok.}$$

The beam is safe in deflection.

Step: ③ Design for flexure [Appendix G pg: No-96]

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$$M_u = 0.87 f_y A_{st} d \left[1 - \frac{f_y \times A_{st}}{f_{ck} b d} \right]$$

$$\Rightarrow 260.46 \times 10^6 = 0.87 \times 415 \times A_{st} \times 600$$

$$\times \left[1 - \frac{415 \times A_{st}}{20 \times 300 \times 600} \right]$$

$$\Rightarrow A_{st} = 1442.04 \text{ mm}^2$$

$$\text{No. of bars required} = \frac{A_{st}}{A_{\phi}} = \frac{1442.04}{314} = 4.59 \approx 5$$

Assume 20 mm dia bars

No. of bars

Provide 5 no-20 mm dia bars. as positive moment reinforcement along the bottom edge of the beam at an effective cover of 50 mm.

$$A_{st} \text{ provided} = 5 \times 314 = 1570 \text{ mm}^2 \left[> 1442.04 \text{ mm}^2 \right]$$

check for A_{st} : [cl: 26.5.1]

$$A_{st \text{ min}} = \frac{0.85 \times b \times d}{f_y} = \frac{0.85 \times 300 \times 600}{415} = 368.67 \text{ mm}^2$$

$$A_{st \text{ max}} = 0.04 \times b \times D = 0.04 \times 300 \times 650 = 7800 \text{ mm}^2$$

$$A_{st \text{ min}} < A_{st} < A_{st \text{ max}} \text{ Hence OK}$$

N/m.
46 kN-m.
KN/m
5 KN/m
beam
tion

Step: ④ Development of Steel/Reinforcement:

(Cl: 26.2.1)

* Required development length for 20 mm dia bar

$$\Rightarrow L_{d \text{ req}} = \frac{\phi \sigma_s}{4 \times \tau_{bd}}$$

$$\Rightarrow L_{d \text{ req}} = \frac{\phi \times 0.87 \times 415}{4 \times (1.2 \times 1.6)}$$

$$\Rightarrow L_{d \text{ req}} = 47 \phi$$

At Mid span

Development length required for positive moment

$$\text{reinforcement} = \left. \begin{array}{l} 47 \phi + 12 \phi \\ \text{or} \\ 47 \phi + d \end{array} \right\} \text{Which is greater}$$

$$\therefore \text{Development length req} = 47 \times 20 + 600 = 1540 \text{ mm}$$

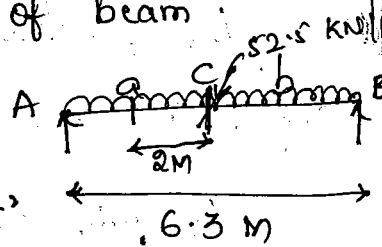
∴ provide the development length of 2 mm on either side of mid span of beam

Moment at 1.15 M from

$$\text{Support } M_b = V_A \times 1.15 - \frac{52.5 \times 1.15^2}{2}$$

$$V_A = \frac{wL}{2} = \frac{52.5 \times 6.3}{2} \Rightarrow M_b = 155.46 \text{ kN-m}$$

$$= 165.4 \text{ kN}$$



$$M_u = 0.87 f_y A_{st} \times d \left[1 - \frac{f_y A_{st}}{f_{ck} b d} \right]$$

$$\Rightarrow 155.46 \times 10^6 = 0.87 \times 415 \times A_{st} \times 600$$

$$\times \left[1 - \frac{415 \times A_{st}}{20 \times 300 \times 600} \right]$$

$$\Rightarrow A_{st} = 789.47 \text{ mm}^2$$

$$\text{No. of bars} = 789.47 / 314$$

$$= 2.51 \approx 3 \text{ no.}$$

∴ 2 no - 20 mm dia bars are curtailed at distance of 2 m on either side of mid span and the remaining steel is continued into the support on same face.

Step: (5) Check for Development length:

$$\text{Development length provided} = 6.3/2 - 2 \text{ m}$$

$$= 3.15 - 2 = 1.15 \text{ m}$$

$$= 1150 \text{ mm.}$$

$$\text{At support } l_d \leq \frac{M}{B} + L_0$$

$$< \frac{47\phi}{3} = 313.3 \text{ mm}$$

$$\text{Where } M = 0.87 f_y A_{st} \times d \left[1 - \frac{f_y A_{st}}{f_{ck} b d} \right]$$

$$\text{Where } A_{st} = 3 \times 314$$

$$= 942 \text{ mm}^2$$

$$\therefore M_u = 0.87 \times 415 \times 942 \times 600 \left[1 - \frac{415 \times 942}{20 \times 300 \times 600} \right]$$

$$\Rightarrow M_u = 181.9 \times 10^6 \text{ kN-m}$$

$$V = \frac{wL}{2} = 165.4 \text{ kN}$$

Initially assume $l_0 = 0$

$$l_d \leq M/BV$$

$$\Rightarrow 47\phi \leq \frac{181.9 \times 10^6}{165.4 \times 10^3}$$

$$\Rightarrow 47\phi \leq 1.09 \times 10^3$$

$$\Rightarrow \phi \leq \frac{1.09 \times 10^3}{47}$$

$$\Rightarrow \phi \leq 23.39 \text{ mm}$$

[20 < 23.39] Hence OK

Provide a 90° bend beyond the center of the support.

$$\text{Anchorage length } l_0 = 8\phi = 8 \times 20 = 160 \text{ mm}$$

Step: (6) Check for shear: [C1: 40]

$$\text{Nominal shear stress} = \tau_v = \frac{V_u}{bd} = \frac{165.4 \times 10^3}{300 \times 600}$$

$$\Rightarrow \tau_v = 0.91 \text{ mpa}$$

$$\text{Design shear stress} = \tau_c = 0.49 \text{ mpa} \quad [\text{from tab}]$$

$$P_t = \frac{100 A_{st}}{bd} = \frac{100 \times 942}{300 \times 600}$$

$$\Rightarrow P_t = 0.52\%$$

Maximum shear capacity $\tau_{c \max} = 2.8 \text{ mpa}$.

$$* \tau_v < \tau_{c \max} \text{ --- OK}$$

$$* \tau_v > \tau_c$$

Assume 8 mm dia 2 legged vertical stirrups

$$A_{sv} = 2 \times \frac{\pi}{4} \times 8^2 = 100.5 \text{ mm}^2$$

$$V_{ue} = V_u - \tau_c b d$$

$$= 165.4 \times 10^3 - 0.49 \times 300 \times 600$$

$$V_{us} = 77.2 \text{ kN}$$

$$S_{v1} = 0.87 f_y A_{sv} d / V_{us}$$

$$= \frac{0.87 \times 415 \times 100.5 \times 600}{77.2 \times 10^3}$$

$$\Rightarrow S_{v1} = 282 \text{ mm}$$

$$S_{v2} = 0.75 d = 0.75 \times 600 = 450 \text{ mm}$$

$$S_{v3} = 300 \text{ mm}$$

∴ provide 8 mm dia 2 legged vertical stirrups at 250 mm center to center.

→ check for A_{sv} :

$$\frac{A_{sv}}{b s_v} \geq \frac{0.4}{0.87 f_y}$$

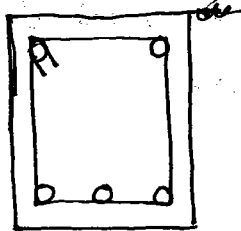
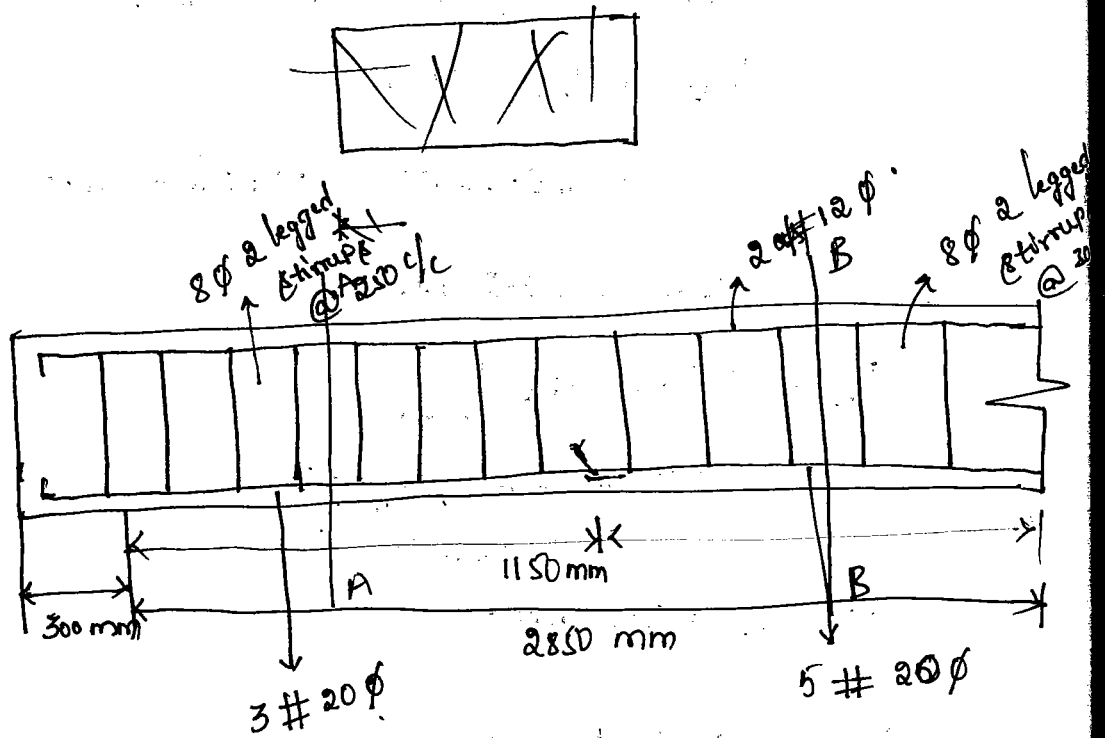
$$\Rightarrow A_{sv} \geq \frac{0.4 \times b \cdot s_v}{0.87 f_y}$$

$$\Rightarrow A_{sv} \geq \frac{0.4 \times 300 \times 280}{0.87 \times 415}$$

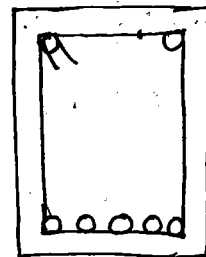
$$\Rightarrow A_{sv} \geq 83 \text{ mm}^2 \quad [< 100.5 \text{ mm}^2]$$

Hence ok

Step: ⑦ Detailing of Reinforcement:



Section A-A



Section B-B